## U.S. WALL GUIDE

Featuring Trus Joist ${ }^{\circledR}$ TimberStrand ${ }^{\circledR}$ LSL and Parallam ${ }^{\circledR}$ PSL Wall Framing

- Engineered to meet code requirements for walls up to 30 ' tall
- Easy-to-use tables adaptable to a variety of wind conditions, surface finishes, and wall layouts
- Out-of-plane wind and vertical load information for designing walls that are stiff, strong, and straight
- Limited product warranty



The products in this guide are readily available through our nationwide network of distributors and dealers. For more information on other applications or other Trus Joist ${ }^{\circledR}$ products, contact your Weyerhaeuser representative.

## Code Evaluations:

See ICC-ES ESR-1387

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## Choose Trus Joist ${ }^{\circledR}$ wall framing for straight, flush walls that:

- are critical for tile applications.
- allow easy countertop and cabinet installation in kitchens and bathrooms.
- give visual appeal to tall walls in great rooms and entryways.
- have the strength and stiffness to accommodate "window" walls.

Many of today's homes have design requirements-such as walls over 10 feet tall-that exceed the code provisions for conventional construction. Trus Joist ${ }^{\circledR}$ TimberStrand ${ }^{\circledR}$ laminated strand lumber (LSL) and Parallam ${ }^{\circledR}$ parallel strand lumber (PSL) can help you meet the requirements of these challenging designs. Weyerhaeuser also offers product and design support that includes technical information, design software, and design advice from our team of skilled engineers and sales representatives.

## Tall wall software solutions

Forte ${ }^{\circledR}$ WEB software is a single-member sizing solution created by Weyerhaeuser to help estimators, architects, and engineers design walls quickly and efficiently. Forte ${ }^{\circledR}$ WEB software provides the most economical solutions for studs, columns, and headers, and helps you design connections for each member. Professional calculations can be printed out for engineer sign-off or to give to building officials. Ask your Weyerhaeuser representative how you can get Forte ${ }^{\circledR}$ WEB software today.

## This guide features the following Trus Joist ${ }^{\circledR}$ wall framing products:

### 1.3E TimberStrand ${ }^{\circledR}$ LSL


Columns: $3^{1} / 2^{\prime \prime} \times 51 / 2^{\prime \prime}$ • $31 / 2^{\prime \prime} \times 71 / 4^{\prime \prime}$
Headers: $31 / 2^{\prime \prime} \times 51 / 2^{\prime \prime}$ • $31 / 2^{\prime \prime} \times 71 / 4^{\prime \prime}$
1.5E TimberStrand ${ }^{\circledR}$ LSL

Studs and Columns: $1 \frac{1}{1} 2^{\prime \prime} \times 7 \frac{1}{4} 4^{\prime \prime}(2 \times 8)$
1.55E TimberStrand ${ }^{\circledR}$ LSL

Studs and Columns: $13 / 4^{\prime \prime} \times 5 \frac{1}{2} 2^{\prime \prime}$ • $13 / 4^{\prime \prime} \times 7 \frac{1}{4} 4^{\prime \prime}$
Headers: $31 / 2^{\prime \prime} \times 91 / 22^{\prime \prime}$ • $31 / 2^{\prime \prime} \times 11 / 8^{\prime \prime}$

Other sizes may be available in Weyerhaeuser software; however, not all products are available in all markets. Contact your Weyerhaeuser representative for the sizes available in your area.

## DEFLECTION REQUIREMENTS

## How stiff does a wall need to be?

While model building codes provide required deflection limits based on the type of finish supported by the wall framing, acceptable deflection limits are usually established by the design professional, finish-material provider, and/or building code authority. Typical deflection requirements are shown in table below.

Code Minimum Deflection Criteria

| Type of Wall | Maximum <br> Deflection |
| :--- | :---: |
| Exterior walls with plaster or stucco finish ${ }^{(1)}$ | $\mathrm{L} / 360^{(5)}$ |
| Exterior walls with brittle finishes ${ }^{(1)(2)}$ | $\mathrm{L} / 240$ |
| Exterior walls with flexible finishes ${ }^{(1)(2)}$ | $\mathrm{L} / 120$ |
| Exterior walls with interior gypsum board finish ${ }^{(3)}$ | $\mathrm{L} / 180$ |
| Members supporting windows $(\text { mullions })^{(4)}$ | $\mathrm{L} / 175$ |

(1) 2009, 2012 and 2015 International Residential Code (IRC), Table R301.7
(2) 2009, 2012 and 2015 International Building Code (IBC), Table 1604.3
(3) 2009, 2012 and 2015 IRC, Table R301.7, footnote d
(4) 2009 IRC, Section R612.11.2; 2012 IRC, Section R612.8.2; 2015 IRC, Section R609.8.2; 2009, 2012 and 2015 IBC, Section 2403.3
(5) For finishes that require a deflection stricter than $L / 360$, contact your Weyerhaeuser representative.

## Limitations of Conventional Construction

> For walls up to $10^{\prime}$ in height, $2 \times 4$ and $2 \times 61.3 E$ TimberStrand ${ }^{\circledR}$ LSL studs may be conventionally specified per the limitations described on this page. Engineered design for more demanding applications is outlined on the pages that follow.

## Wind Limitations

Basic wind speed (2009):
< 100 mph in hurricane-prone regions;
< 110 mph elsewhere per IRC Section R301.2.1.1
Basic wind speed (2012 and 2015):
Figure R301.2(4)B

## Seismic Design Categories

$A, B, C, D_{0}, D_{1}$, and $D_{2}$. Excludes irregular portions of structures as defined by IRC R301.2.2.2.5


## -

Mean roof height limited to 33' measured from average grade to average roof elevation, or per local zoning ordinance

## Limitation Descriptions and IRC References

| Description | 2009, 2012 and 2015 IRC References |
| :--- | :--- | :--- | (1) Maximum roof span, including overhangs, limited to 40'. Maximum tabulated rafter span | (horizontal projection) and ceiling joist span of 26'. |
| :--- | | R802.10.2.1; footnote a to IRC Tables R802.4(1), R802.4(2); |
| :--- |
| footnote bto IRC Tables R802.5.1(1)-R802.5.1(8) |,

## Stud Specifications for Conventional Applications per IRC Table R602.3(5)

| Stud <br> Size | Laterally <br> unsupported stud <br> height(1) | Maximum spacing when <br> supporting roof and <br> ceiling only | Maximum spacing when <br> supporting one floor, <br> roof, and ceiling | Maximum spacing when <br> supporting two floors, <br> roof, and ceiling | Maximum spacing <br> when supporting <br> one floor only | Laterally <br> unsupported stud <br> height ${ }^{(1)}$ | Maximum <br> spacing |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\prime}$ | $24^{\prime \prime}$ | $16^{\prime \prime}$ | - | $24^{\prime \prime}$ | $14^{\prime \prime}$ | $24^{\prime \prime}$ |
|  | $10^{\prime}$ | $24^{\prime \prime}$ | $24^{\prime \prime}$ | $16^{\prime \prime}$ | $24^{\prime \prime}$ | $20^{\prime}$ | $24^{\prime \prime}$ |

[^0]When used in conventional construction applications, both $2 \times 4$ and $2 \times 6$ TimberStrand ${ }^{\circledR}$ LSL studs may be drilled or notched in accordance with IRC Section R602.6.

Buckling Length—Distance along the length of a member between braced points. This length is used to calculate the buckling stability of the member.

Conventional Construction-Generally, home design based on traditional construction methods and materials that have a history of adequate structural performance for specific building types and sizes. Both conventionally specified and pre-calculated members and connections are prescriptively specified in building codes such as the IRC and IBC, and may be combined to form a structure or structural assemblage.

Design Wind Pressure-The equivalent static wind pressure applied to structures to determine wind loads for buildings.

Effective Wind Area-The area used to determine external wind coefficients. These coefficients are used in the determination of the design wind pressures for components and cladding elements. Generally, the effective wind area is the length of a member's span times the tributary width or $L / 3$, whichever is greater.

Lateral Loads-Loads applied to a structure in the horizontal direction. This includes loads from wind and seismic events.

Main Force Resisting System—Structural elements designated to provide support and stability for the overall structure. The system generally receives wind loading from more than one surface.
Tributary Area-A calculated area of influence surrounding a structural member. Loads within this area are added together to determine the amount of load a member is required to resist. For example, the tributary area for a wall stud is the sum of $1 / 2$ the distance to the adjacent wall stud on each side of the stud in question. Likewise, the tributary area for a floor joist would be the sum of $1 / 2$ the distance to the adjacent joist on each side of the joist in question.

## ENGINEERED DESIGN ASSUMPTIONS

Design applications are limited to vertical loads, and to lateral wind loads that are perpendicular to the wall framing. Table information is based on the strength calculations and deflection limits of wall framing members, and was generated with the following assumptions:

- Member design and lateral support requirements for bending are based on National Design Specification ${ }^{\circledR}($ (NDS®).
- Stud and column tables assume structural sheathing on one side of the wall, or a combination of gypsum wallboard and non-structural sheathing or siding applied to each side of the wall, or equivalent.
- Blocking required at 8' on-center maximum per code. See page 12.
- Column bracing assumed to be 8 ' on-center maximum. Stud bracing at $1^{1}$ on-center maximum.
- Beams and columns must remain straight to within $552 / 4608$ (in.) of true alignment. $L$ is the unrestrained length of the member in feet.
- If stud spacing is 19.2 or 24 " on-center, trusses or rafters must be installed within 3 " of the stud locations. This does not apply if studs are spaced at 16 " on-center or less.
- The Components \& Cladding (C\&C) pressures shown in the Wall Design Wind Pressure table below are used only for strength calculations.
- Deflection limits are based on Main Wind Force Resisting System pressures, which were estimated by multiplying the C\&C pressure by 0.70 (2009, 2012 and 2015 IRC Table R301.7 and IBC Table 1604.3).
- $\Delta=\frac{270 \mathrm{wL}^{4}}{E b d}+\frac{28.8 \mathrm{wL}^{2}}{E b d}$
$\Delta=$ deflection
$\mathrm{w}=$ uniform load (plf)
$\mathrm{L}=\operatorname{span}(\mathrm{ft})$
b = member width (in.)
$\mathrm{d}=$ member depth (in.)
E = modulus of elasticity (psi)


## WIND TABLES

## Wall Design Wind Pressure (PSF) ${ }^{(1)(2)}$

| Exposure Category ${ }^{(3)}$ | Effective Wind Area ${ }^{(4)}$ (ft ${ }^{2}$ ) | Basic Wind Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2009 IRC/IBC or Older (ASCE 7-05: W) |  |  |  |  |  |  |  | 2012 and 2015 IRC/IBC (ASCE 7-10: 0.6W) |  |  |  |  |  |  |  |  |
|  |  | 85 | 90 | 100 | 110 | 120 | 130 | 140 | 150 | 110 | 115 | 120 | 130 | 140 | 150 | 160 | 170 | 180 |
| B | $\leq 10$ | 14.5 | 16.2 | 20.1 | 24.3 | 28.9 | 33.9 | 39.3 | 45.1 | 14.6 | 15.9 | 17.3 | 20.3 | 23.6 | 27.1 | 30.8 | 34.8 | 39.0 |
|  | 50 | 13.1 | 14.7 | 18.1 | 21.9 | 26.1 | 30.6 | 35.5 | 40.8 | 13.2 | 14.4 | 15.7 | 18.4 | 21.3 | 24.5 | 27.8 | 31.4 | 35.2 |
|  | $\geq 100$ | 12.5 | 14.0 | 17.3 | 20.9 | 24.9 | 29.2 | 33.9 | 38.9 | 12.5 | 13.7 | 14.9 | 17.5 | 20.3 | 23.3 | 26.6 | 30.0 | 33.6 |
| C | $\leq 10$ | 20.1 | 22.6 | 27.9 | 33.7 | 40.1 | 47.1 | 54.6 | 62.7 | 20.3 | 22.1 | 24.1 | 28.3 | 32.8 | 37.7 | 42.9 | 48.4 | 54.3 |
|  | 50 | 18.2 | 20.4 | 25.2 | 30.5 | 36.2 | 42.5 | 49.3 | 56.6 | 18.3 | 20.0 | 21.8 | 25.6 | 29.7 | 34.0 | 38.7 | 43.7 | 49.0 |
|  | $\geq 100$ | 17.3 | 19.4 | 24.0 | 29.1 | 34.6 | 40.6 | 47.1 | 54.0 | 17.5 | 19.1 | 20.8 | 24.4 | 28.3 | 32.5 | 37.0 | 41.7 | 46.8 |
| D | $\leq 10$ | 23.7 | 26.6 | 32.9 | 39.8 | 47.3 | 55.5 | 64.4 | 73.9 | 23.9 | 26.1 | 28.4 | 33.4 | 38.7 | 44.4 | 50.6 | 57.1 | 64.0 |
|  | 50 | 21.5 | 24.1 | 29.7 | 35.9 | 42.8 | 50.2 | 58.2 | 66.8 | 21.6 | 23.6 | 25.7 | 30.2 | 35.0 | 40.1 | 45.7 | 51.6 | 57.8 |
|  | $\geq 100$ | 20.5 | 22.9 | 28.3 | 34.3 | 40.8 | 47.9 | 55.5 | 63.7 | 20.6 | 22.5 | 24.5 | 28.8 | 33.4 | 38.3 | 43.6 | 49.2 | 55.2 |

(1) Tabulated pressures are based on the Analytical Procedure defined in ASCE 7. Values assume a Components and Cladding (C\&C) member in the interior zone of an enclosed structure, with the following factors:

- Risk/occupancy category II
- Topographical factor of 1.0
- Mean roof height of 33'
(2) When designing in accordance with 2012 and 2015 IRC/IBC, the load combinations include a 0.6 factor for wind. Tabulated wind pressures in the 2012 and 2015 IRC/IBC portion of this table are reduced by 0.6 for direct use with the 2009 IRC-based load tables in this guide.
(3) Exposure categories are generally defined as follows (see ASCE 7):

B = Urban and suburban areas, wooded areas
$C=0$ pen terrain with scattered obstructions generally less than $30^{\prime}$ in height
$D=$ Flat, unobstructed areas
(4) Effective Wind Area is the span times the tributary width or $L^{2} / 3$, whichever is greater. For values of effective wind areas not listed, interpolation between $10 \mathrm{ft}^{2}$ and $100 \mathrm{ft}^{2}$ is allowed.

## Effective Wind Area

- Check local codes for any special wind pressures.

When designing in accordance with the 2012 or 2015 IRC/IBC, use the load tables in this guide in conjunction with the 2012 and 2015 IRC/IBC wind pressures above, which have been reduced by 0.6 .

| Wall <br> Height | Stud/Column <br> Effective Wind Area (ft${ }^{2}$ ) |
| :---: | :---: |
| $\geq \mathbf{1 8 ^ { \prime }}$ | 100 |
| $1 \mathbf{6}^{\prime}$ | 85 |
| $14^{\prime}$ | 65 |
| $1 \mathbf{2}^{\prime}$ | 48 |
| $10^{\prime}$ | 33 |

- Values are based on L2/3 with a maximum of $100 \mathrm{ft}^{2}$.
- The effective wind area should not be confused with the tributary area, which is used to determine the amount of load applied to an individual member.


## Given

- Wall height $=20^{\prime}$
- Rough opening $=6^{\prime}$
- Exposure Category "B"
- 140 mph basic wind speed
- 2015 IRC/IBC
- Flexible exterior finish with interior gypsum board finish; walls support window mullions
- Maximum column vertical load $=5,000 \mathrm{lbs}$
- Maximum header vertical load $=250 \mathrm{plf}$

When designing with C\&C pressures, the effective wind area ( $\mathrm{L}^{2} / 3$ ) helps determine the wall design wind pressure. A smaller effective wind area results in a higher wind pressure. The effective wind area should not be confused with the tributary area, which is used to determine the amount of load applied to an individual member.

## 1. Determine effective wind areas ( $\mathrm{ft}^{2}$ ):

- For the studs and columns, refer to the Effective Wind Area table on page 4. A 20 ' stud or column will have an effective wind area of $100 \mathrm{ft}^{2}$.
- For each header, consult the drawing at right and use the maximum value of the rough opening ( L ) times the tributary width or L²/3, whichever is greater.
- For the top header in our example wall, use the maximum of either ( $6^{\prime} \times 5^{\prime}=30 \mathrm{ft}^{2}$ ) or $\left(6^{2} / 3=12 \mathrm{ft}^{2}\right)$.
- For the bottom header in our example wall, use the maximum of either ( $6^{\prime} \times 10^{\prime}=60 \mathrm{ft}^{2}$ ) or ( $6^{2} / 3=12 \mathrm{ft}^{2}$ ).

The effective wind areas calculate to $30 \mathrm{ft}^{2}$ for the top header and $60 \mathrm{ft}^{2}$ for the bottom header, so interpolation would be required to find exact pressures. For simplicity, we will use an effective wind area of $10 \mathrm{ft}^{2}$ for each header. This allows us to skip the interpolation exercise, and provides a more conservative wind pressure.
2. Determine design wind pressure: Consult the Wall Design Wind Pressure table on page 4, using the example wall's criteria of Exposure B, a 140 mph basic wind speed, and an effective wind area as calculated above:

- For studs/columns with an effective area of $100 \mathrm{ft}^{2}$, the wall design lateral wind pressure is 20.3 psf .
- For headers with an effective area of $10 \mathrm{ft}^{2}$, the wall design wind pressure is 23.6 psf .

3. Determine appropriate deflection criteria: Consult the Code Minimum Deflection Criteria on page 2. Our example wall contains both windows (minimum $\mathrm{L} / 175$ ) and a flexible finish with interior gypsum board (minimum $\mathrm{L} / 180$ ). Because the $\mathrm{L} / 180$ deflection is more restrictive, the wall should be designed using the $\mathrm{L} / 180$ deflection values in this guide.


A complete wall specification should include permanent bracing, safety bracing, blocking, connections, details, etc. See pages 11-14.

Refer to stud, column, and header tables on pages 6-10 to design the components for this example wall.

## ONE-HOUR WALL ASSEMBLY WITH TIMBERSTRAND® ${ }^{\circledR}$ LSL STUDS

$2 \times 6$ Wall Application: $2 \times 6$ wall made with TimberStrand ${ }^{\circledR}$ LSL studs and gypsum wallboard applied horizontally. $2 \times 6$ or larger TimberStrand ${ }^{\circledR}$ LSL is permitted as a substitute in fire-rated assemblies when used in the same or larger dimensions as sawn lumber.

## TimberStrand LSL Wall Assembly

1. $2 \times 6$ TimberStrand ${ }^{\circledR}$ LSL studs, spaced $16^{\prime \prime}$ on-center, with double top plates and single bottom plate
2. $5 / 8$ " Type $X$ gypsum wallboard, $4^{\prime}$ wide, applied horizontally. Horizontal joints are unblocked. Horizontal application of wallboard represents the direction of least fire resistance as opposed to vertical application.
3. $2^{1 / 4} / 4$ " $\# 6$ Type $S$ drywall screws, spaced along stud at $7 "$ on-center and covered with joint compound
4. Wallboard joints covered with paper tape and joint compound

- The design axial compressive stress within the TimberStrand ${ }^{\circledR}$ LSL studs must not exceed the least of the following:
- 435 psi
$-F_{c} \times 0.30$, where $F_{c}$ is the compression design value parallel-to-grain for the TimberStrand ${ }^{\circledR}$ LSL, adjusted by all applicable adjustment factors (in accordance with the NDS®), including the column stability factor $\mathrm{C}_{p}$
- $F_{c} \times 0.30$, where $F_{c}$ is caclulated in accordance with the NDS ${ }^{\circledR}$, assuming a slenderness ratio $\mathrm{Le}_{\mathrm{e}} / \mathrm{d}$ of 21


## This assembly has been tested to ASTM E119/NFPA 251 and CAN/ULC-S101 Standards.



Top View (plates not shown)


## STUD LOAD TABLE AND EXAMPLE

Studs—Maximum Allowable Lateral (Wind) and Vertical Load

| Wall | Load and Deflection | 1.3 T TimberStrand ${ }^{\text {® }}$ LSL |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $11 / 2^{17} \times 1 / 2^{\prime \prime}$ |  |  |  | $11 / 2^{\prime \prime} \times 1 / 1 / 2$ |  |  |  |  |  | $\text { 11/2" x } 71 / 41$ |  |  |  |  |  |
|  |  | Lateral Load (plf) |  |  |  | Lateral Load (plf) |  |  |  |  |  |  Lateral Load (plf)    <br> 15 20 $266^{(1)}$ 30  |  |  |  |  |  |
|  |  | 15 | 20 | $26^{(1)}$ | 30 | 15 | 20 | $26^{(1)}$ | 30 | 40 | 50 |  |  |  |  | 40 | 50 |
| $8^{\prime}$ | Vertical (lbs) | 2,745 | 2,590 | 2,405 | 2,280 | 4,385 | 4,385 | 4,385 | 4,385 | 4,385 | 4,385 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 |
|  | Defl. Ratio | L/677 | L/508 | L/391 | L/339 | L/2,553 | L/1,915 | L/1,473 | L/1,277 | L/958 | L/766 | L/6,518 | L/4,888 | L/3,760 | L/3,259 | L/2,444 | L/1,955 |
| 91 | Vertical (lbs) | 2,175 | 2,010 | 1,820 | 1,690 | 4,385 | 4,385 | 4,385 | 4,385 | 4,385 | 4,385 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 |
|  | Defl. Ratio | L/478 | L/358 | L/276 | L/239 | L/1,812 | L/1,359 | L/1,045 | L/906 | L/679 | L/543 | L/4,656 | L/3,492 | L/2,686 | L/2,328 | L/1,746 | L/1,397 |
| 10' | Vertical (lbs) | 1,730 | 1,560 | 1,360 | 1,230 | 4,385 | 4,385 | 4,385 | 4,385 | 4,385 | 4,385 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 |
|  | Defl. Ratio | L/349 | L/262 | L/202 | L/175 | L/1,330 | L/998 | L/767 | L/665 | L/499 | L/399 | L/3,437 | L/2,577 | L/1,983 | L/1,718 | L/1,289 | L/1,031 |
| 11' | Vertical (lbs) | 1,380 | 1,205 | 1,005 | 870 | 4,385 | 4,385 | 4,385 | 4,385 | 4,230 | 3,775 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 |
|  | Defl. Ratio | L/263 | L/197 | L/152 | L/132 | L/1,005 | L/754 | L/580 | L/502 | L/377 | L/301 | L/2,606 | L/1,955 | L/1,503 | L/1,303 | L/977 | L/782 |
| 12' | Vertical (lbs) | 1,100 | 925 |  |  | 4,385 | 4,375 | 4,085 | 3,890 | 3,415 | 2,940 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 |
|  | Defl. Ratio | L/203 | L/152 |  |  | L/777 | L/583 | L/448 | L/389 | L/291 | L/233 | L/2,022 | L/1,516 | L/1,166 | L/1,011 | L/758 | L/606 |
| 13' | Vertical (lbs) | 870 |  |  |  | 3,980 | 3,725 | 3,420 | 3,220 | 2,725 | 2,230 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 |
|  | Defl. Ratio | L/160 |  |  |  | L/613 | L/460 | L/354 | L/307 | L/230 | L/184 | L/1,599 | L/1,199 | L/922 | L/799 | L/600 | L/480 |
| 14' | Vertical (lbs) | 690 |  |  |  | 3,435 | 3,165 | 2,855 | 2,650 | 2,135 | 1,620 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 |
|  | Defl. Ratio | L/128 |  |  |  | L/492 | L/369 | L/284 | L/246 | L/185 | L/148 | L/1,286 | L/964 | L/742 | L/643 | L/482 | L/386 |
| 15' | Vertical (lbs) |  |  |  |  | 2,965 | 2,690 | 2,370 | 2,160 | 1,635 | 1,095 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 |
|  | Defl. Ratio |  |  |  |  | L/401 | L/301 | L/231 | L/201 | L/150 | L/120 | L/1,049 | L/787 | L/605 | L/525 | L/393 | L/315 |
| 16' | Vertical (lbs) |  |  |  |  | 2,560 | 2,285 | 1,960 | 1,745 | 1,205 |  | 5,775 | 5,775 | 5,775 | 5,775 | 5,775 | 5,245 |
|  | Defl. Ratio |  |  |  |  | L/331 | L/248 | L/191 | L/166 | L/124 |  | L/867 | L/650 | L/500 | L/434 | L/325 | L/260 |
| 17' | Vertical (lbs) |  |  |  |  | 2,210 | 1,930 | 1,605 | 1,385 |  |  | 5,775 | 5,775 | 5,775 | 5,625 | 5,020 | 4,425 |
|  | Defl. Ratio |  |  |  |  | L/276 | L/207 | L/159 | L/138 |  |  | L/725 | L/543 | L/418 | L/362 | L/272 | L/217 |
| 18' | Vertical (lbs) |  |  |  |  | 1,910 | 1,630 | 1,295 |  |  |  | 5,775 | 5,565 | 5,180 | 4,930 | 4,315 | 3,705 |
|  | Defl. Ratio |  |  |  |  | L/233 | L/175 | L/135 |  |  |  | L/612 | L/459 | L/353 | L/306 | L/229 | L/184 |
| 19' | Vertical (lbs) |  |  |  |  | 1,650 | 1,365 |  |  |  |  | 5,295 | 4,960 | 4,570 | 4,315 | 3,690 | 3,070 |
|  | Defl. Ratio |  |  |  |  | L/198 | L/149 |  |  |  |  | L/521 | L/391 | L/301 | L/261 | L/195 | L/156 |
| 20' | Vertical (lbs) |  |  |  |  | 1,420 | 1,135 |  |  |  |  | 4,765 | 4,425 | 4,030 | 3,775 | 3,140 | 2,505 |
|  | Defl. Ratio |  |  |  |  | L/170 | L/128 |  |  |  |  | L/447 | L/336 | L/258 | L/224 | L/168 | L/134 |
| 21' | Vertical (lbs) |  |  |  |  | 1,220 |  |  |  |  |  | 4,295 | 3,950 | 3,550 | 3,290 | 2,650 |  |
|  | Defl. Ratio |  |  |  |  | L/147 |  |  |  |  |  | L/387 | L/290 | L/223 | L/193 | L/145 |  |
| 22' | Vertical (lbs) |  |  |  |  | 1,040 |  |  |  |  |  | 3,875 | 3,525 | 3,125 | 2,860 | 2,210 |  |
|  | Defl. Ratio |  |  |  |  | L/128 |  |  |  |  |  | L/337 | L/253 | L/194 | L/168 | L/126 |  |
| 23' | Vertical (lbs) |  |  |  |  |  |  |  |  |  |  | 3,495 | 3,150 | 2,745 | 2,480 |  |  |
|  | Defl. Ratio |  |  |  |  |  |  |  |  |  |  | L/295 | L/221 | L/170 | L/148 |  |  |
| 24' | Vertical (lbs) |  |  |  |  |  |  |  |  |  |  | 3,160 | 2,810 | 2,400 | 2,135 |  |  |
|  | Defl. Ratio |  |  |  |  |  |  |  |  |  |  | L/260 | L/195 | L/150 | L/130 |  |  |
| 25' | Vertical (lbs) |  |  |  |  |  |  |  |  |  |  | 2,855 | 2,505 | 2,095 |  |  |  |
|  | Defl. Ratio |  |  |  |  |  |  |  |  |  |  | L/230 | L/173 | L/133 |  |  |  |
| 26' | Vertical (lbs) |  |  |  |  |  |  |  |  |  |  | 2,580 | 2,230 |  |  |  |  |
|  | Defl. Ratio |  |  |  |  |  |  |  |  |  |  | L/205 | L/154 |  |  |  |  |
| 27' | Vertical (lbs) |  |  |  |  |  |  |  |  |  |  | 2,330 | 1,980 |  |  |  |  |
|  | Defl. Ratio |  |  |  |  |  |  |  |  |  |  | L/183 | L/137 |  |  |  |  |
| 28' | Vertical (lbs) |  |  |  |  |  |  |  |  |  |  | 2,105 | 1,755 |  |  |  |  |
|  | Defl. Ratio |  |  |  |  |  |  |  |  |  |  | L/164 | L/123 |  |  |  |  |
| 29' | Vertical (lbs) |  |  |  |  |  |  |  |  |  |  | 1,900 |  |  |  |  |  |
|  | Defl. Ratio |  |  |  |  |  |  |  |  |  |  | L/148 |  |  |  |  |  |
| 30' | Vertical (lbs) |  |  |  |  |  |  |  |  |  |  | 1,715 |  |  |  |  |  |
|  | Defl. Ratio |  |  |  |  |  |  |  |  |  |  | L/134 |  |  |  |  |  |

(1) Load based on a wind pressure of 19.1 psf and studs spaced at 16 " on-center.

## General Notes

- Table is based on:
- A load duration factor of 1.60 .
- Stud bracing in Engineered Design Assumptions on page 4.
- A buckling length coefficient of $K_{e}=0.85$. For deflection, use $K_{e}=1.0$.
- Axial loads applied eccentrically, at a distance of $1 / 6$ of the wall thickness dimension of the stud, measured from the stud centerline.
- A compression perpendicular-to-grain stress of 425 psi, adjusted per NDS® ${ }^{\circledR}$ 3.10.4.
- A code-allowed repetitive-member increase of $4 \%$.


## Stud Example

For the Design Example on page 5, design 20' studs for lateral wind pressure of 20.3 psf and a maximum vertical load of 250 plf:

- Determine the maximum stud length:

The maximum stud length in this example wall is $20^{\prime}$.

- Calculate the lateral load in plf:

This example uses 16 " on-center studs, so calculate the lateral load in plf and the vertical load in Ibs as follows:
$20.3 \mathrm{psf} \times 16 / 12=27.1 \mathrm{plf} ; 250 \mathrm{plf} \times 16 / 12=333 \mathrm{lbs}$.

- Select the appropriate studs:

In the Stud Load Table, scan across the 20 ' row until you find a cell in the

## STUD LOAD TABLE AND EXAMPLE

Studs—Maximum Allowable Lateral (Wind) and Vertical Load continued

| $\begin{array}{\|l\|l} \hline \text { Wall } \\ \text { Ht. } \end{array}$ | Load and Deflection | 1.55E TimberStrand ${ }^{\text {® }}$ LSL |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $13 / 4 \mathrm{x} \times 1 / 2^{\prime \prime}$ |  |  |  |  |  | 13/4" $\times 71 / 4{ }^{\text {" }}$ |  |  |  |  |  |
|  |  | Lateral Load (plf) |  |  |  |  |  | Lateral Load (plf) |  |  |  |  |  |
|  |  | 15 | 20 | $26^{(1)}$ | 30 | 40 | 50 | 15 | 20 | $26^{(1)}$ | 30 | 40 | 50 |
| $8^{\prime}$ | Vertical (lbs) | 4,965 | 4,965 | 4,965 | 4,965 | 4,965 | 4,965 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 |
|  | Defl. Ratio | L/3,552 | L/2,664 | L/2,049 | L/1,776 | L/1,332 | L/1,066 | L/7,857 | L/5,893 | L/4,533 | L/3,929 | L/2,946 | L/2,357 |
| 9' | Vertical (lbs) | 4,965 | 4,965 | 4,965 | 4,965 | 4,965 | 4,965 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 |
|  | Defl. Ratio | L/2,520 | L/1,890 | L/1,454 | L/1,260 | L/945 | L/756 | L/5,613 | L/4,210 | L/3,238 | L/2,807 | L/2,105 | L/1,684 |
| 10' | Vertical (lbs) | 4,965 | 4,965 | 4,965 | 4,965 | 4,965 | 4,965 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 |
|  | Defl. Ratio | L/1,851 | L/1,388 | L/1,068 | L/925 | L/694 | L/555 | L/4,143 | L/3,107 | L/2,390 | L/2,072 | L/1,554 | L/1,243 |
| 11' | Vertical (lbs) | 4,965 | 4,965 | 4,965 | 4,965 | 4,965 | 4,965 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 |
|  | Defl. Ratio | L/1,398 | L/1,048 | L/806 | L/699 | L/524 | L/419 | L/3,142 | L/2,356 | L/1,813 | L/1,571 | L/1,178 | L/943 |
| 12' | Vertical (lbs) | 4,965 | 4,965 | 4,965 | 4,965 | 4,965 | 4,965 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 |
|  | Defl. Ratio | L/1,081 | L/811 | L/624 | L/541 | L/405 | L/324 | L/2,437 | L/1,828 | L/1,406 | L/1,219 | L/914 | L/731 |
| 13' | Vertical (lbs) | 4,965 | 4,965 | 4,965 | 4,965 | 4,950 | 4,500 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 |
|  | Defl. Ratio | L/853 | L/640 | L/492 | L/427 | L/320 | L/256 | L/1,928 | L/1,446 | L/1,112 | L/964 | L/723 | L/578 |
| 14' | Vertical (lbs) | 4,965 | 4,965 | 4,795 | 4,600 | 4,130 | 3,670 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 |
|  | Defl. Ratio | L/685 | L/514 | L/395 | L/342 | L/257 | L/205 | L/1,550 | L/1,163 | L/894 | L/775 | L/581 | L/465 |
| 15' | Vertical (lbs) | 4,670 | 4,410 | 4,110 | 3,915 | 3,435 | 2,965 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 |
|  | Defl. Ratio | L/558 | L/418 | L/322 | L/279 | L/209 | L/167 | L/1,265 | L/949 | L/730 | L/632 | L/474 | L/379 |
| 16' | Vertical (lbs) | 4,095 | 3,830 | 3,530 | 3,330 | 2,845 | 2,365 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 |
|  | Defl. Ratio | L/461 | L/345 | L/266 | L/230 | L/173 | L/138 | L/1,045 | L/784 | L/603 | L/523 | L/392 | L/314 |
| 17' | Vertical (lbs) | 3,600 | 3,335 | 3,025 | 2,825 | 2,335 |  | 6,550 | 6,550 | 6,550 | 6,550 | 6,550 | 5,950 |
|  | Defl. Ratio | L/385 | L/288 | L/222 | L/192 | L/144 |  | L/874 | L/655 | L/504 | L/437 | L/328 | L/262 |
| 18' | Vertical (lbs) | 3,170 | 2,905 | 2,595 | 2,395 | 1,900 |  | 6,550 | 6,550 | 6,550 | 6,335 | 5,710 | 5,095 |
|  | Defl. Ratio | L/324 | L/243 | L/187 | L/162 | L/122 |  | L/737 | L/553 | L/425 | L/369 | L/277 | L/221 |
| 19' | Vertical (lbs) | 2,800 | 2,530 | 2,220 | 2,020 |  |  | 6,550 | 6,260 | 5,860 | 5,600 | 4,965 | 4,340 |
|  | Defl. Ratio | L/276 | L/207 | L/159 | L/138 |  |  | L/628 | L/471 | L/362 | L/314 | L/236 | L/188 |
| 20' | Vertical (lbs) | 2,470 | 2,205 | 1,895 |  |  |  | 5,965 | 5,620 | 5,215 | 4,950 | 4,305 | 3,675 |
|  | Defl. Ratio | L/237 | L/178 | L/137 |  |  |  | L/539 | L/405 | L/311 | L/270 | L/202 | L/162 |
| 21' | Vertical (lbs) | 2,185 | 1,920 |  |  |  |  | 5,400 | 5,045 | 4,640 | 4,375 | 3,725 | 3,080 |
|  | Defl. Ratio | L/205 | L/154 |  |  |  |  | L/467 | L/350 | L/269 | L/233 | L/175 | L/140 |
| 22' | Vertical (lbs) | 1,935 | 1,670 |  |  |  |  | 4,895 | 4,540 | 4,125 | 3,860 | 3,205 | 2,550 |
|  | Defl. Ratio | L/178 | L/134 |  |  |  |  | L/406 | L/305 | L/234 | L/203 | L/152 | L/122 |
| 23' | Vertical (lbs) | 1,715 |  |  |  |  |  | 4,440 | 4,080 | 3,670 | 3,400 | 2,740 |  |
|  | Defl. Ratio | L/156 |  |  |  |  |  | L/356 | L/267 | L/205 | L/178 | L/133 |  |
| 24' | Vertical (lbs) | 1,515 |  |  |  |  |  | 4,035 | 3,675 | 3,260 | 2,990 |  |  |
|  | Defl. Ratio | L/137 |  |  |  |  |  | L/313 | L/235 | L/181 | L/157 |  |  |
| 25' | Vertical (lbs) | 1,340 |  |  |  |  |  | 3,665 | 3,305 | 2,890 | 2,620 |  |  |
|  | Defl. Ratio | L/122 |  |  |  |  |  | L/278 | L/208 | L/160 | L/139 |  |  |
| 26' | Vertical (lbs) |  |  |  |  |  |  | 3,335 | 2,975 | 2,560 | 2,285 |  |  |
|  | Defl. Ratio |  |  |  |  |  |  | L/247 | L/185 | L/142 | L/123 |  |  |
| 27' | Vertical (lbs) |  |  |  |  |  |  | 3,035 | 2,675 | 2,260 |  |  |  |
|  | Defl. Ratio |  |  |  |  |  |  | L/221 | L/165 | L/127 |  |  |  |
| 28' | Vertical (lbs) |  |  |  |  |  |  | 2,765 | 2,405 |  |  |  |  |
|  | Defl. Ratio |  |  |  |  |  |  | L/198 | L/148 |  |  |  |  |
| 29' | Vertical (lbs) |  |  |  |  |  |  | 2,520 | 2,160 |  |  |  |  |
|  | Defl. Ratio |  |  |  |  |  |  | L/178 | L/134 |  |  |  |  |
| 30' | Vertical (lbs) |  |  |  |  |  |  | 2,295 | 1,935 |  |  |  |  |
|  | Defl. Ratio |  |  |  |  |  |  | L/161 | L/121 |  |  |  |  |

(1) Load based on a wind pressure of 19.1 psf and studs spaced at $16^{\mathrm{\prime} \mathrm{\prime}}$ on-center.

## Stud Example continued from page 6

30 plf Lateral Load column that meets the L/180 deflection and the 333 lbs vertical load criteria. According to the table, a 1.3 E TimberStrand ${ }^{\circledR}$ LSL $2 \times 6$ stud is not an option. If the stud spacing is changed to 12" on-center (for a plf of 20.3), it still would not meet the L/180 requirement. However, a 1.5E TimberStrand ${ }^{\circledR}$ LSL $2 \times 8$ stud (at $3,775 \mathrm{lbs}$ and $\mathrm{L} / 224$ ) spaced at $16^{\prime \prime}$ on-center meets the requirements, making it the best option for this wall.

- Design stud connections:

Convert 27.1 plf into a reaction (uniform load x length/2): $27.1\left(20^{\prime} / 2\right)=271 \mathrm{lbs}$. Use the Lateral Connections tables on page 13 to select a nail or angle clip connection that meets or exceeds 271 lbs . For this example a nailed connection can be calculated as $271 / 104=2.61$, so three $16 \mathrm{~d}\left(0.131^{\prime \prime} \times 31 / 4^{\prime \prime}\right)$ nails (nailed through the plate into the end grain) would work. For an angle clip connection, one Simpson Strong-Tie ${ }^{\circledR}$ A34 angle clip at the top and bottom plate is sufficient.


Columns—Maximum Allowable Lateral (Wind) Load (PLF)/Vertical Load (Ibs)

| Defl. Ratio | Wall Ht. | Max. Defl. | 31/2" Wall Thickness |  |  |  |  |  | 51⁄2" Wall Thickness |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | TimberStrand ${ }^{\text {® }}$ LSL |  |  | Parallam ${ }^{\text {® }}$ PSL |  |  | TimberStrand ${ }^{\text {® }}$ LSL |  |  | Parallam ${ }^{\text {® }}$ PSL |  |  |  |
|  |  |  | 1.3 E |  |  | 1.8 E |  |  | 1.3 E |  | 1.55 E | 1.8E |  |  | 2.0 E |
|  |  |  | $\begin{aligned} & \hline \text { Double } \\ & 2 \times 4(1) \end{aligned}$ | $\begin{gathered} 5^{51 / 2 " x ~ x ~} 3 / 2{ }^{12} \\ \text { (Plank) } \end{gathered}$ | $\begin{gathered} 71 / 4 " \times 31 / 21 \\ \text { (Plank) } \end{gathered}$ | $31 / 2 \times 31 / 2$ " | $51 / 4 " \times 31 / 21$ <br> (Plank) | $7 \mathrm{x} \mathrm{x} \mathrm{3} 1 / 21$ <br> (Plank) | $\begin{aligned} & \hline \text { Double } \\ & 2 \times 6^{(1)} \end{aligned}$ | $31 / 2$ " $51 / 2{ }^{\text {" }}$ | $\begin{array}{\|c} \hline \text { Double } \\ 13 / 44^{\prime \prime} \times 51 / 2^{(1)} \end{array}$ | $31 / 2 \mathrm{x} \times 51 / 4$ | 51/4" x $51 / 4$ " | 7" x 51⁄4" (Plank) | 91/4" $\times 51 / 4 "$ (Plank) |
| L/360 | $30^{\prime}$ | 1.00" |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 28' | 0.93" |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 26 | 0.87" |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 24' | 0.80" |  |  |  |  |  |  |  |  |  |  |  | 23/8,165 | 33/11,675 |
|  | $22^{\prime}$ | 0.73" |  |  |  |  |  |  |  |  |  |  | 22/7,070 | 30/9,385 | 44/13,235 |
|  | 20 | 0.67" |  |  |  |  |  |  |  |  |  |  | 29/8,235 | 39/10,955 | 58/15,165 |
|  | $18^{\prime}$ | 0.60" |  |  |  |  |  |  |  | 22/5,110 | 2716,030 | 27/6,375 | 40/9,655 | 54/12,830 | 80/17,295 |
|  | 16' | 0.53" |  |  |  |  |  | 23/5,510 | 27/3,620 | 32/5,985 | 38/6,410 | 38/7,580 | 58/11,400 | 77/15,220 | 113/18,765 |
|  | 14' | 0.47" |  |  | 25/5,075 |  | 25/5,160 | 34/6,850 | 41/3,640 | 47/6,890 | 57/6,630 | 5717,810 | 86/11,715 | 115/15,620 | 169/19,800 |
|  | 12' | 0.40" |  | 31/4,840 | 40/6,415 | 2714,350 | 40/6,540 | 54/8,695 | 64/3,625 | 75/7,300 | 90/6,720 | 91/7,810 | 136/11,715 | 182/15,620 | 267/20,590 |
|  | 10' | 0.33" | 29/2,345 | 53/6,300 | 70/8,300 | 47/5,205 | 70/7,810 | 94/10,415 | 110/3,515 | 129/7,450 | 154/6,655 | 156/7,810 | 234/11,715 | 300/15,620 | 300/20,640 |
|  | $8^{\prime}$ | 0.27" | 56/2,360 | 103/8,180 | 136/10,785 | 91/5,205 | 136/7,810 | 182/10,415 | 212/3,285 | 248/7,215 | 295/6,390 | 300/7,810 | 300/11,715 | 300/15,620 | 300/20,640 |
| L/240 | 30 | 1.50" |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 28' | 1.40" |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 26' | 1.30 " |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 24' | 1.20" |  |  |  |  |  |  |  |  |  |  | 26/5,535 | 34/7,425 | 50/10,570 |
|  | 22' | 1.10 " |  |  |  |  |  |  |  |  | 2214,220 | 22/4,210 | 33/6,360 | 45/8,420 | 66/11,890 |
|  | 201 | 1.00" |  |  |  |  |  |  | 21/2,970 | 24/3,855 | 29/4,870 | 29/4,855 | 44/7,315 | 59/9,730 | 87/13,510 |
|  | 18' | 0.90" |  |  |  |  |  |  | 29/3,065 | 34/4,370 | 40/5,355 | 40/5,610 | 61/8,440 | 81/11,270 | 120/15,215 |
|  | 16' | 0.80" |  |  | 25/3,720 |  | 26/3,750 | 34/5,030 | 41/3,125 | 48/5,060 | 57/5,615 | 58/6,480 | 87/9,825 | 116/13,100 | 170/16,975 |
|  | 14' | 0.70" |  | 29/3,430 | 38/4,530 | 25/3,100 | 38/4,630 | 51/6,160 | 61/3,105 | 71/5,660 | 85/5,750 | 86/7,545 | 129/11,525 | 173/15,315 | 254/18,370 |
|  | 12' | 0.60" | 25/1,985 | 46/4,265 | 61/5,605 | 40/3,860 | 61/5,755 | 81/7,685 | 97/2,985 | 113/5,775 | 135/5,705 | 136/7,810 | 205/11,715 | 273/15,620 | 300/20,590 |
|  | 10' | 0.50" | 43/2,055 | 80/5,355 | 105/7,075 | 70/4,870 | 105/7,310 | 141/9,710 | 166/2,750 | 194/5,545 | 231/5,460 | 234/7,805 | 300/11,715 | 300/15,620 | 300/20,640 |
|  | $8^{\prime}$ | 0.40" | 84/2,005 | 155/6,760 | 204/8,920 | 136/5,205 | 205/7,810 | 273/10,410 | 300/2,465 | 300/6,215 | 300/6,340 | 300/7,810 | 300/11,715 | 300/15,620 | 300/20,640 |
| L/180 | 30 | 2.00" |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 281 | 1.87" |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 26' | 1.73 " |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 24' | 1.60" |  |  |  |  |  |  |  |  | 22/3,385 | 23/3,305 | 34/5,035 | 46/6,670 | 67/9,535 |
|  | 22' | 1.47" |  |  |  |  |  |  | 21/2,485 | 24/2,985 | 29/3,805 | 30/3,725 | 45/5,640 | 60/7,515 | 88/10,620 |
|  | 201 | 1.33" |  |  |  |  |  |  | 28/2,585 | 33/3,295 | 39/4,305 | 39/4,270 | 59/6,445 | 79/8,575 | 117/11,885 |
|  | 18' | 1.20" |  |  |  |  |  |  | 38/2,660 | 45/3,720 | 54/4,655 | 54/4,830 | 81/7,335 | 109/9,725 | 160/13,220 |
|  | 16' | 1.07" |  | 26/2,530 | 34/3,345 | 23/2,270 | 34/3,425 | 46/4,545 | 55/2,620 | 64/4,155 | 76/4,840 | 77/5,470 | 116/8,300 | 155/11,050 | 227/14,435 |
|  | 14' | 0.93" | 21/1,630 | 39/3,035 | 51/4,015 | 34/2,755 | 51/4,130 | 68/5,510 | 82/2,515 | 95/4,435 | 114/4,825 | 115/6,095 | 173/9,335 | 230/12,485 | 300/16,640 |
|  | 12' | 0.80" | 33/1,745 | 62/3,675 | 81/4,870 | 54/3,360 | 81/5,040 | 109/6,690 | 129/2,300 | 151/4,200 | 180/4,630 | 182/6,035 | 273/10,210 | 300/15,620 | 300/20,590 |
|  | $10^{\prime}$ | 0.67" | 58/1,740 | 106/4,470 | 140/5,880 | 94/4,080 | 141/6,125 | 188/8,165 | 221/1,835 | 258/3,455 | 300/4,260 | 300/5,750 | 300/11,715 | 300/15,620 | 300/20,640 |
|  | $8^{\prime}$ | 0.53" | 112/1,620 | 206/5,170 | 272/6,800 | 182/4,375 | 273/7,250 | 282/10,415 | 300/2,465 | 300/6,215 | 300/6,340 | 300/7,810 | 300/11,715 | 300/15,620 | 300/20,640 |

(1) For 3-ply and 4-ply built-up columns, multiply table values by 1.5 and 2.0 , respectively. See page 11 for connection requirements.

- Green numbers refer to lateral (wind) load (PLF). Black numbers refer to vertical load (lbs).


## General Notes

- Tables are based on:
- A load duration factor of 1.60 .
- Full-width blocking at a maximum vertical spacing of 8' on-center.
- A buckling length coefficient of $K_{e}=0.85$. For deflection use $K_{e}=1.0$.
- Axial loads applied eccentrically, at a distance of $1 / 6$ of the wall thickness dimension of the column, measured from the column centerline.
- A compression perpendicular-to-grain stress of 425 psi .
- Solid sections required where specified. Built-up columns require reductions. Contact your Weyerhaeuser representative for assistance.

Beam Orientation


Plank Orientation


Some columns are listed in both beam and plank orientation. The first dimension is for member width, and the second dimension is for member depth (wall thickness).

## TimberStrand ${ }^{\otimes}$ LSL and untreated Parallam ${ }^{\oplus}$ PSL are intended for dry-use applications

Columns—Maximum Allowable Lateral (Wind) Load (PLF)/Vertical Load (Ibs)

| Defl. Ratio | Wall Ht . | Max. Defl. | 7114" Wall Thickness |  |  |  |  |  |  | $\begin{gathered} \hline 91 / 4 \text { " Wall Thickness } \\ \hline \text { Parallam®PSL } \\ \hline 2.0 \mathrm{E} \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | TimberStrand ${ }^{\text {® }}$ LSL |  |  | Parallam ${ }^{\text {® }}$ PSL |  |  |  |  |  |
|  |  |  | 1.5 E | 1.3 E | 1.55 E |  | 1.8 E |  | 2.0 E |  |  |
|  |  |  | $\begin{gathered} \hline \text { Double } \\ 2 \times 88^{11)} \end{gathered}$ | $31 / 2 \mathrm{x} \times 71 / 4$ " | $\begin{array}{\|c\|} \hline \text { Double } \\ 13 / 4 \times 71 / 4^{11} \end{array}$ | $3112{ }^{1} \times 7$ " | 5114" $\times 7$ " | 7" x 7 " | $91 / 4 \text { " x } 7 \text { " }$ (Plank) | $31 / 2^{\prime \prime} \times 91 / 4 "$ | 51/4"x 91/4" |
| L/360 | $30^{\prime}$ | 1.00" |  |  |  |  | 21/8,945 | 28/11,960 | 41/16,925 | 35/12,095 | 53/18,180 |
|  | 28' | 0.93" |  |  |  |  | 25/10,045 | 34/13,370 | 50/18,725 | 43/12,560 | 65/18,875 |
|  | $26^{\prime}$ | 0.87" |  |  | 2017,255 | 21/7,445 | 32/11,195 | 43/14,945 | 63/20,655 | 54/12,965 | 82/19,485 |
|  | $24^{\prime}$ | 0.80" | 21/5,505 | 21/6,555 | 26/7,800 | 2718,365 | 40/12,675 | 54/16,905 | 80/22,795 | 69/13,240 | 104/20,010 |
|  | $22^{\prime}$ | 0.73" | 28/5,595 | 2817,345 | 33/8,220 | 35/9,485 | 53/14,295 | 70/19,185 | 103/24,515 | 90/13,385 | 135/20,460 |
|  | 20' | 0.67" | 3775,685 | 3718,360 | 44/8,505 | 47/10,415 | 70/15,620 | 94/20,825 | 138/25,645 | 119/13,505 | 179/20,640 |
|  | 18' | 0.60" | 50/5,730 | 51/9,005 | 61/8,665 | 64/10,415 | 96/15,620 | 128/20,825 | 188/26,585 | 162/13,605 | 244/20,640 |
|  | 16' | 0.53" | 72/5,685 | 73/9,370 | 8778,730 | 91/10,415 | 136/15,620 | 182/20,825 | 267/27,350 | 230/13,685 | 282/20,640 |
|  | 14' | 0.47" | 107/5,595 | 108/9,580 | 129/8,690 | 135/10,415 | 202/15,620 | 270/20,825 | 300/27,520 | 300/13,750 | 300/20,640 |
|  | 12' | 0.40" | 168/5,430 | 170/9,510 | 203/8,500 | 212/10,415 | 300/15,620 | 300/20,825 | 300/27,520 | 300/13,760 | 300/20,640 |
|  | 10' | 0.33" | 286/5,140 | 289/9,080 | 300/8,640 | 300/10,415 | 300/15,620 | 300/20,825 | 300/27,520 | 300/13,760 | 300/20,640 |
|  | $8^{\prime}$ | 0.27" | 300/6,010 | 300/10,785 | 300/9,965 | 300/10,415 | 300/15,620 | 300/20,825 | 300/27,520 | 300/13,760 | 300/20,640 |
| L/240 | 30' | 1.50" |  |  | 20/5,195 | 21/5,300 | 31/8,050 | 42/10,720 | 61/15,230 | 53/10,640 | 80/16,210 |
|  | 28' | $1.40{ }^{\prime \prime}$ | 20/4,560 | 20/4,600 | 24/5,805 | 25/5,930 | 38/8,920 | 51/11,920 | 75/16,705 | 65/11,280 | 98/17,215 |
|  | $26^{\prime}$ | 1.30" | 25/4,740 | 25/5,090 | 30/6,460 | 32/6,525 | 48/9,870 | 64/13,220 | 94/18,290 | 82/11,775 | 123/18,040 |
|  | $24^{\prime}$ | 1.20" | 324,865 | 32/5,635 | 39/6,860 | 40/7,325 | 61/11,005 | 81/14,775 | 120/19,960 | 104/12,100 | 156/18,750 |
|  | $22^{\prime}$ | 1.10" | 42/4,925 | 42/6,230 | 50/7,175 | 53/8,105 | 79/12,325 | 106/16,475 | 155/21,690 | 135/12,105 | 202/19,225 |
|  | $20^{\prime}$ | 1.00" | 55/4,990 | 56/6,910 | 6777,340 | 70/9,100 | 105/13,815 | 141/18,465 | 207/23,155 | 179/11,960 | 226/20,640 |
|  | 18' | 0.90" | 76/4,940 | 7717,265 | 92/7,405 | 96/9,890 | 144/15,455 | 192/20,760 | 251/25,880 | 244/11,620 | 251/20,640 |
|  | 16' | 0.80" | 108/4,830 | 109/7,370 | 130/7,370 | 136/10,165 | 205/15,620 | 273/20,825 | 282/27,350 | 282/12,865 | 282/20,640 |
|  | 14' | 0.70" | 160/4,630 | 162/7,190 | 193/7,145 | 202/10,095 | 300/15,620 | 300/20,825 | 300/27,520 | 300/13,750 | 300/20,640 |
|  | 12' | 0.60" | 252/4,285 | 255/6,600 | 300/6,755 | 300/10,155 | 300/15,620 | 300/20,825 | 300/27,520 | 300/13,760 | 300/20,640 |
|  | 10' | 0.50" | 300/5,015 | 300/8,820 | 300/8,640 | 300/10,415 | 300/15,620 | 300/20,825 | 300/27,520 | 300/13,760 | 300/20,640 |
|  | $8^{\prime}$ | 0.40" | 300/6,010 | 300/10,785 | 300/9,965 | 300/10,415 | 300/15,620 | 300/20,825 | 300/27,520 | 300/13,760 | 300/20,640 |
| L/180 | 30' | 2.00 " | 22/3,825 | 22/3,655 | 26/4,710 | 28/4,710 | 42/7,130 | 56/9,560 | 82/13,555 | 71/9,110 | 107/13,975 |
|  | $28^{\prime}$ | 1.87" | 274,035 | 27/3,995 | 32/5,175 | 34/5,190 | 51/7,865 | 68/10,545 | 101/14,720 | 87/9,535 | 131/14,670 |
|  | $26^{\prime}$ | 1.73" | 34/4,145 | 34/4,340 | 41/5,625 | 43/5,650 | 64/8,615 | 86/11,505 | 126/15,970 | 109/9,810 | 164/15,150 |
|  | $24^{\prime}$ | 1.60" | 43/4,240 | 43/4,745 | 52/5,965 | 54/6,245 | 81/9,490 | 109/12,665 | 160/17,230 | 139/9,835 | 188/16,730 |
|  | 22' | 1.47" | 56/4,260 | 56/5,140 | 67/6,155 | 70/6,845 | 106/10,345 | 141/13,930 | 205/18,540 | 180/9,600 | 205/19,060 |
|  | $20^{\prime}$ | 1.33" | 74/4,245 | 75/5,485 | 89/6,230 | 94/7,390 | 141/11,280 | 188/15,180 | 226/22,080 | 226/9,755 | 226/20,640 |
|  | 18' | 1.20" | 101/4,140 | 103/5,515 | 122/6,160 | 128/7,780 | 192/12,215 | 251/16,810 | 251/25,880 | 251/11,355 | 251/20,640 |
|  | 16' | 1.07" | 144/3,900 | 146/5,240 | 174/5,895 | 182/7,575 | 273/12,785 | 282/20,825 | 282/27,350 | 282/12,865 | 282/20,640 |
|  | 14' | 0.93" | 214/3,520 | 216/4,575 | 258/5,405 | 270/6,905 | 300/15,620 | 300/20,825 | 300/27,520 | 300/13,750 | 300/20,640 |
|  | 12' | 0.80" | 300/3,530 | 300/4,855 | 300/6,755 | 300/10,155 | 300/15,620 | 300/20,825 | 300/27,520 | 300/13,760 | 300/20,640 |
|  | 10' | 0.67" | 300/5,015 | 300/8,820 | 300/8,640 | 300/10,410 | 300/15,620 | 300/20,825 | 300/27,520 | 300/13,760 | 300/20,640 |
|  | $8^{\prime}$ | 0.53" | 300/6,010 | 300/10,785 | 300/9,965 | 300/10,410 | 300/15,620 | 300/20,825 | 300/27,520 | 300/13,760 | 300/20,640 |

(1) For 3-ply and 4-ply built-up columns, multiply table values by 1.5 and 2.0 , respectively. See page 11 for connection requirements.

- Green numbers refer to lateral (wind) load (PLF). Black numbers refer to vertical load (lbs).


## Column Example

For the Design Example wall on page 5, design $20^{\prime}$ columns for lateral wind pressure of 20.3 psf and vertical loading of $5,000 \mathrm{lbs}$ :

Note: Vertical load is the load applied to the top of the column, excluding the header reaction. The header reaction is assumed to transfer directly to the trimmers.

- Calculate the lateral load in plf:

The calculated wind pressure in the example is 20.3 psf , so $20.3 \times 3.67$ ' tributary width $=74.5$ plf.

- Select an appropriate column:

Scan the L/180 section of the Column Load Tables to find a 20 ' column that meets or exceeds the 74.5 plf lateral load and the $5,000 \mathrm{lbs}$ vertical load. For this example, a 7 " $\times 51 / 4$ " 1.8 E Parallam ${ }^{\circledR}$ PSL column (at $79 / 8,575$ ), used in plank orientation, will work for a $2 \times 6$ wall. Alternatively, a double $13 / 4$ " $\times 71 / 4$ " 1.55 E TimberStrand ${ }^{\circledR}$ LSL column (at $89 / 6,230$ ) would work for a $2 \times 8$ wall.

- Design the column to wall plate connections:

Convert 74.5 plf into a reaction (uniform load $x$ length $/ 2$ ): $74.5\left(20^{\prime} / 2\right)=745 \mathrm{lbs}$. Use the Lateral Connections tables on page 13 to select a connection that meets or exceeds 745 lbs . For this example $745 / 465=1.60$; so according to the Angle Clips table, two Simpson Strong-Tie ${ }^{\circledR}$ A34 connectors would be required-one on each side of the column, at both the top and bottom plates.


Headers—Maximum Allowable Lateral (Wind) Load (PLF)/Vertical Load (PLF)

| Lateral Defl. Ratio | Rough Opening | Max. Defl. | $\begin{gathered} \hline \text { 31/2" Wall Thickness } \\ \hline \text { TimberStrand }{ }^{\circledR} \\ \text { LSL } \end{gathered}$ |  |  |  | 51/2" Wall Thickness |  |  | 71/4" Wall Thickness <br> TimberStrand ${ }^{\circledR}$ <br> LSL <br> $1.3 E$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | $\begin{gathered} \hline \text { TimberStrand }{ }^{\oplus} \\ \text { LSL } \end{gathered}$ | $\begin{aligned} & \text { Parallam® } \\ & \text { PSL } \end{aligned}$ |  |  |
|  |  |  | 1.3 E |  | 1.55 E |  | 1.3 E | 1.8 E | 2.0 E |  |
|  |  |  | $31 / 2 \mathrm{x} \times 51 / 2 \mathrm{~L}$ | $31 / 2^{\prime \prime} \times 71 / 4^{\prime \prime}$ | $31 / 2 \mathrm{x} \times 11 / 2$ | $31 / 2 \mathrm{x} \times 111 / 8{ }^{\text {" }}$ |  | $51 / 4 \mathrm{x} \times{ }^{11 / 4}{ }^{\text {" }}$ | 51/4" $\times 91 / 4$ " | $\begin{gathered} 71 / 4 \times 31 / 2 " 4 \\ \text { (Plank) } \end{gathered}$ |
| L/360 | 12' | 0.41" | 30/30 | 40/80 | 60/215 | 75/335 |  | 130/60 | 250/385 |  |
|  | $10^{\prime}$ | 0.34" | 50/70 | 65/165 | $100 / 435$ | $130 / 535$ | 120/25 | 220/130 | 425/785 | 270/35 |
|  | $9 '$ | 0.31" | 65/110 | 90/250 | 140/575 | 175/695 | 165/40 | 295/200 | 490/1,170 | 365/55 |
|  | $8^{1}$ | 0.28" | 95/175 | 125/395 | 195/765 | 245/925 | 225/70 | 410/320 | 50011,605 | 500/90 |
|  | 7' | 0.24" | 140/295 | 180/650 | 285/1,040 | 31011,220 | 330/120 | 500/535 | 50011,830 | 500/160 |
|  | $6^{1}$ | 0.21" | 215/525 | 280/895 | 36011,420 | 3601,415 | $500 / 220$ | 500/955 | 500/2,125 | 500/290 |
|  | $5{ }^{\prime}$ | 0.18" | 355/690 | 43011,230 | 43011,690 | 4301,685 | 500/370 | 500/1,525 | 500/2,535 | 500/485 |
|  | $4^{\prime}$ | $0.14{ }^{\text {" }}$ | 50011,125 | 50011,995 | 500/2,090 | 500/2,085 | 500/685 | 500/2,060 | 500/3,135 | 500/900 |
|  | $3^{\prime}$ | 0.11" | 50022,020 | 500/2,740 | 500/2,735 | 500/2,735 | 500/1,340 | 500/2,930 | 500/4,105 | 500/1,770 |
| L/240 | 12' | 0.61" | 45/30 | $60 / 80$ | 90/215 | 115/295 |  | 195/60 | 370/385 |  |
|  | $10^{\prime}$ | 0.51" | 75/70 | 100/165 | 155/380 | $190 / 460$ | 180/25 | 325/130 | $440 / 785$ | 405/35 |
|  | $9^{\prime}$ | 0.46" | 100/110 | 135/250 | $210 / 485$ | 245/605 | 245/40 | 440/200 | 490/1,170 | 490/55 |
|  | $8^{1}$ | 0.41" | 140/175 | 185/395 | 275/655 | 275/885 | 340/70 | 500/320 | 50011,605 | 500/90 |
|  | $7{ }^{\prime}$ | 0.36" | 210/295 | 275/540 | 31011,000 | 3101,220 | 495/95 | 500/535 | 50011,830 | 500/160 |
|  | $6^{1}$ | 0.31" | 320/380 | $360 / 750$ | 36011,420 | 3601,415 | 500/220 | 500/955 | 500/2,125 | 500/290 |
|  | $5{ }^{\prime}$ | 0.26" | 430/580 | 43011,230 | 43011,690 | 4301,685 | 500/370 | 500/1,525 | 500/2,535 | 500/485 |
|  | $4^{\prime}$ | 0.21" | 50011,125 | 5001,995 | 500/2,090 | 500/2,085 | 500/685 | 500/2,060 | 500/3,135 | 500/900 |
|  | $3^{\prime}$ | $0.16{ }^{\prime \prime}$ | 50022,020 | 500/2,740 | 500/2,735 | 500/2,735 | 500/1,340 | 500/2,930 | 500/4,105 | 500/1,770 |
| L/180 | $12^{\prime}$ | 0.82" | 60/30 | 75/80 | $120 / 210$ | 150/255 |  | 255/60 | 370/385 |  |
|  | $10^{\prime}$ | 0.68" | 100/70 | 130/165 | 205/325 | 220/430 | 240/25 | 435/130 | $440 / 785$ | 440/35 |
|  | $9^{\prime}$ | 0.62" | 135/110 | 175/250 | 245/440 | 245/605 | 325/40 | 490/200 | 490/1,170 | 490/55 |
|  | $8^{1}$ | 0.55" | 190/175 | 250/340 | 275/655 | 275/885 | 455/25 | 500/320 | 50011,605 | 500/90 |
|  | $7^{\prime}$ | 0.48" | 275/225 | 310/470 | 31011,000 | 31011,220 | 500/90 | 500/535 | 50011,830 | 500/160 |
|  | $6^{\prime}$ | 0.42" | 360/320 | $360 / 750$ | 360/1,420 | 360/1,415 | 500/220 | 500/955 | 500/2,125 | 500/290 |
|  | $5{ }^{\prime}$ | 0.35" | 430/580 | 43011,230 | 43011,690 | 43011,685 | 500/370 | 500/1,525 | 500/2,535 | 500/485 |
|  | $4^{\prime}$ | 0.28" | 50011,125 | 5001,995 | 500/2,090 | 500/2,085 | 500/685 | 500/2,060 | 500/3,135 | 500/900 |
|  | $3^{\prime}$ | 0.22" | 5002, 2020 | 500/2,740 | 500/2,735 | 500/2,735 | 500/1,340 | 500/2,930 | 500/4,105 | 500/1,770 |

" Bold italic values require two trimmers (3" bearing) at ends. Single trimmers may work for lightly loaded bold italic sections; see table below.

- Green numbers refer to lateral (wind) load (PLF). Black numbers refer to vertical load (PLF).


## General Notes

- Table is based on:
- A load duration factor of 1.60 for combined lateral and vertical load.
- A load duration factor of 1.00 for vertical load only.
- Uniform lateral (wind) and vertical loads (beam weight considered).
- Vertical deflection, the more restrictive of $\mathrm{L} / 240$ or $5 / 16^{\prime \prime}$.
- A maximum lateral (wind) load of 500 plf.


## Bearing Requirements

- Trimmers must support the full width of the header.
- Minimum header support to be one trimmer ( $11 / 2$ ") at ends.

Maximum Allowable
Vertical Load (PLF) with One Trimmer

| Rough <br> Opening | Wall Thickness |  |
| :---: | ---: | ---: |
|  | $\mathbf{3} \mathbf{1 / 2} \mathbf{2}^{\mathbf{\prime}}$ | $\mathbf{5} \mathbf{1 / 2}$ |
| $\mathbf{1 2}^{\mathbf{\prime}}$ | 355 | 536 |
| $\mathbf{1 0}^{\mathbf{\prime}}$ | 428 | 646 |
| $\mathbf{9}^{\mathbf{\prime}}$ | 476 | 718 |
| $\mathbf{8}^{\mathbf{\prime}}$ | 536 | 808 |
| $\mathbf{7}^{\mathbf{\prime}}$ | 613 | 924 |
| $\mathbf{6}^{\mathbf{\prime}}$ | 716 | 1,077 |
| $\mathbf{5}^{\mathbf{\prime}}$ | 858 | 1,290 |
| $\mathbf{4}^{\mathbf{\prime}}$ | 1,069 | 1,607 |
| $\mathbf{3}^{\mathbf{\prime}}$ | 1,415 | 2,126 |

## Header Example

The Design Example on page 5 assumes that both headers will be the same size, and considers worst-case loading. Design the headers for lateral wind pressure of 23.6 psf based on the lower header's 6 ' rough opening and 10 ' tributary width, and a vertical load based on the upper header's maximum 250 plf.

- Calculate the lateral load in plf:

The calculated wind pressure in the example is 23.6 psf , so $23.6 \times 10^{\prime}$ tributary width $=236$ plf.

- Select the appropriate header:

Scan the L/180 section of the Header Load Table to find a header that meets your requirements ( 236 plf lateral and 250 plf vertical). For this example, a $6^{\prime}$ header of $51 / 4$ " $\times 51 / 4$ " 1.8 E Parallam ${ }^{\circledR}$ PSL (at $500 / 955$ ) will work for a $2 \times 6$ wall. Alternatively, a 7114 " x $31 / 2$ " 1.3 E TimberStrand ${ }^{\circledR}$ LSL header (at $500 / 290$ ), used in plank orientation, will work for a $2 \times 8$ wall. Since the table numbers for these selections are not bold, only one trimmer stud is required for bearing. Headers that do not match the wall thickness must be directly attached to a plate that matches the wall thickness to provide lateral bracing. See detail L13 on page 12.

- Design header to column connections:

Convert 236 plf into a reaction (uniform load x length/2): $236\left(6^{\prime} / 2\right)=708 \mathrm{lbs}$. Use the Lateral Connections tables on page 13 to select a connection that meets or exceeds 708 lbs . For this example $708 / 465=1.53$; so according to the Angle Clips connections table on page 13, two Simpson Strong-Tie ${ }^{\circledR}$ A34 connectors are sufficient-one on top and bottom at each end of both headers.


## MULTIPLE-MEMBER CONNECTIONS

## 2-Ply Nailing Recommendations

- For $2 \times 4,13 / 4^{\prime \prime} \times 51 / 2^{\prime \prime}, 2 \times 6,13 / 4$ " $711 / 4^{\prime \prime}$, and $2 \times 8$ : Minimum of two rows of $16 \mathrm{~d}(0.131$ " $\times 31 / 4$ ") pneumatic nails at 10 " on-center, staggered.
- Nail from one side.


## 3-Ply Nailing Recommendations

- For $2 \times 4$ : Minimum of two rows of $16 d$ ( $0.131^{\prime \prime} \times 31 / 4$ ") pneumatic nails at 8" on-center, staggered.
- For $13 / 4^{\prime \prime} \times 51 / 2^{\prime \prime}, 2 \times 6,13 / 4$ " $71 / 4^{\prime \prime}$, and $2 \times 8$ : Minimum of three rows of $16 \mathrm{~d}(0.131 " \times 31 / 4)$ ) pneumatic nails at 5 " on-center, staggered.
- Nail from both sides.


## 4-Ply Fastening Recommendations

- For $2 \times 4$ : Nail each ply to the other with a minimum of two rows of $16 \mathrm{~d}\left(0.131^{\prime \prime} \times 31 / 4\right.$ ") pneumatic nails at 5 " on-center. When connecting each ply, offset nail rows by 2" from the ply below.
- For $13 / 4^{\prime \prime} \times 51 / 2^{\prime \prime}, 2 \times 6,13 / 4^{\prime \prime} \times 71 / 4^{\prime \prime}$, and $2 \times 8$ :
- Nail each ply to the other with a minimum of three rows of 16d ( 0.131 " x 31/4") pneumatic nails at 5 " on-center. When connecting each ply, offset nail rows by 2" from the ply below.
or,
- Minimum of two rows of $1 / 21$ diameter bolts spaced at 8 " on-center.



## CAUTION:

Wrap is slippery when wet or icy
Align stickers (2x3 or larger) directly
over support blocks
Use support blocks ( $6 \times 6$ or larger) at $10^{\prime}$ on-center to keep bundles out of mud and water

Wall reinforcement is required at all lift points to ensure wall stability during construction

## Wind Brace

Details shown are applicable for 90 mph (2009 IRC/IBC) or 115 mph (2012 and 2015 IRC/IBC) basic wind speeds and the exposure categories and maximum wall heights shown in the table below. For other conditions, contact your Weyerhaeuser representative.


* Load 1 value from Lateral Connections-Angle Clips table below.


WB3

* Load 2 value from Lateral Connections—Angle Clips table below.

Wind Brace Detail Applicability

| Detail | Exposure | Max. Wall Height |
| :---: | :---: | :---: |
| WB2 | D | $25^{\prime}$ |
|  | B, C | $29^{\prime}$ |
| WB3 | B, C | $20^{\prime}(1)$ |

(1) Maximum wall height shown includes depth of truss.

## FRAMING CONNECTORS

## Lateral Connections-Nails

| Nail Size | End Grain | Toe Nail |
| :---: | :---: | :---: |
| 8d (0.113" x 2½) | 77 lbs | 96 lbs |
| 10d (0.128" x 3") | 99 lbs | 123 lbs |
| 12d (0.128" x 31⁄4") | 99 lbs | 123 lbs |
| 16d (0.135" x 31⁄2") | 110 lbs | 137 lbs |
| 16d (0.131" x 314") | 104 lbs | 129 lbs |

## General Notes

- Tables are based on a load duration factor of 1.60.
- Connection values based on a specific gravity of 0.50 .
- For end-grain connections, a 0.67 factor was used (based on NDS®).
- For toenail connections, a 0.83 factor was used (based on NDS ${ }^{\circledR}$ ).




A34


## Lateral Connections-Angle Clips

| Type | Nails | Length of Connector <br> (L) | Load 1: Allowable Load (lbs) | Load 2: Allowable Load (lbs) |
| :---: | :---: | :---: | :---: | :---: |
| Simpson Strong-Tie ${ }^{\circledR}$ |  |  |  |  |
| A21 | Four 10d (0.148" $\times 1112^{\prime \prime}$ ) | $13 / 8$ " | 150 | 330 |
| A34 | Eight 8d (0.131" x 112") | 21/2" | 465 | 430 |
| A35 | Twelve 8d (0.131" $\times 1122^{\prime \prime}$ ) | 41/2" | 650 | 670 |
| A23 | Eight 10d (0.148" $\times 1122^{\prime \prime}$ ) | 23/4" | 535 | 680 |
| USP Structural Connectors ${ }^{\circledR}$ |  |  |  |  |
| AC5 | Six 10d (0.148" $\times 1$ ¹2 $2^{\prime \prime}$ ) | $47 / 8^{\prime \prime}$ | 554 | 554 |
| A3 | Eight 10d (0.148" x 1¹⁄2") | 23/4" | 740 | 610 |
| AC7 | Eight 10d (0.148" x 1½") | 615/16" | 740 | 740 |
| AC9 | Ten 10d (0.148" x 1½") | 87/8" | 926 | 882 |

1.55E TimberStrand ${ }^{\circledR}$ LSL Headers and Beams


Other Trus Joist ${ }^{\circledR}$ Headers and Beams


DO NOT cut, notch, or drill holes in headers or beams except as indicated in the illustrations and tables above

## Allowable Holes and Notches* for TimberStrand ${ }^{\circledR}$ LSL Studs

Per ICC ES ESR-1387, holes may be drilled anywhere along the length of the stud but must be at least $5 / 8^{\prime \prime}$ from the edge


## General Notes

- Allowed hole zone suitable for headers and beams with uniform and/or concentrated loads anywhere along the member.
- Round holes only.
- No holes in headers or beams in plank orientation.


### 1.55E TimberStrand ${ }^{\text {® }}$ LSL

| Header or <br> Beam Depth | Maximum Round <br> Hole Size |
| :---: | :---: |
| $\mathbf{9}^{1 / 2}$ | $3^{\prime \prime}$ |
| $11^{1 / 8^{\prime \prime}}$ | $35 / 8^{\prime \prime}$ |
| $\mathbf{1 4}-16^{\prime \prime}$ | $45 / 8^{\prime \prime}$ |

- See illustration for allowed hole zone.


## General Notes

- Allowed hole zone suitable for headers and beams with uniform loads only.
- Round holes only.
- No holes in cantilevers.
- No holes in headers or beams in plank orientation.


## Other Trus Joist ${ }^{\circledR}$ Beams

| Header or <br> Beam Depth | Maximum Round <br> Hole Size |
| :---: | :---: |
| $\mathbf{5}^{1 / 2}$ | $1^{3 / 4^{\prime \prime}}$ |
| $\mathbf{7 1 / 4}-\mathbf{2 0}$ | $2^{\prime \prime}$ |

- See illustration for allowed hole zone.

[^1]

Allowable Design Stresses (100\% Load Duration)

| Grade MOE (x106) (psi) | $\begin{gathered} \mathbf{E}_{\text {min }}{ }^{(1)} \\ (\mathrm{psi}) \end{gathered}$ | Axial |  | Joist/Beam |  |  | Plank |  |  | Equivalent Specific Gravity for Connections |  |  | Min. Shear Wall Nail Spacing ${ }^{(5)}$ (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \mathbf{F}_{\mathrm{cll}} \\ (\mathrm{psi}) \end{gathered}$ | $\begin{aligned} & F_{t^{(2)}} \\ & (\mathrm{psi}) \end{aligned}$ | $\begin{aligned} & \mathbf{F}_{b^{(3)}} \\ & (\mathrm{psi}) \end{aligned}$ | $\underset{(\mathrm{psi})}{\mathbf{F}_{v}}$ | $\begin{aligned} & \mathbf{F}_{\mathrm{c} L^{(4)}} \\ & (\mathrm{psi}) \end{aligned}$ | $\begin{gathered} \mathbf{F}_{b} \\ (\mathrm{psi}) \end{gathered}$ | $\underset{(\mathrm{psi})}{\mathbf{F}_{v}}$ | $\begin{aligned} & \mathbf{F}_{\mathrm{c},}{ }^{(4)} \\ & (\mathrm{psi}) \end{aligned}$ | Lateral | Withdrawal | Shear Walls(5) |  |
| TimberStrand ${ }^{\text {® }}$ LSL |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.3 | 660,750 | 1,835 | 1,300 | 1,700 ${ }^{(6)}$ | 425 | 710 | 1,900 | 150 | $635{ }^{(11)}$ | 0.50 | 0.42 | $0.42^{(7)}$ | $6^{(7)}$ |
| 1.5 | 762,400 | 2,105 | 1,815 | 2,250(6) | 505 | 860 | 2,525 | 150 | 750 |  |  | 0.42 | 2 |
| 1.55 | 787,815 | 2,170 | 1,290(8) | 2,325(6) | $310^{(8)}$ | 900 | 2,615 | 150 | 775 |  |  | 0.42 | 2 |
| Parallam ${ }^{\text {® }}$ PSL |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.8 | 914,880 | 2,500 | 1,995 | 2,500 ${ }^{(9)}$ | 230 | 545 | 2,400 ${ }^{(9)}$ | 190 | 545 | 0.50 | 0.50 | N.A. | N.A. |
| 2.0 | 1,016,535 | 2,900(10) | 2,300 | 2,900 ${ }^{(9)}$ | 290 | 625 | 2,650 ${ }^{(9)}$ | 210 | 635 |  |  |  |  |

(1) Reference modulus of elasticity for beam and column stability calculations per NDS®.
(2) Referenced tension design values are based on a standard 4 foot length. For lengths longer than 4 foot, multiply $F_{t}$ by the following adjustment (where $L$ is length in feet):

$$
\text { -TimberStrand }{ }^{\circledR} \text { LSL (4/L)0.083 } \quad \text {-Parallam }{ }^{\circledR} \text { PSL: }(4 / L)^{0.056}
$$

(3) When structural members qualify as repetitive members in accordance with the applicable building code, a 4\% increase is permitted for $F_{b}$ in addition to the increases permitted in Footnotes 6 and 9.
(6) For 12 " depth. For depths $<31 / 2$ ", use the $31 / 2$ " factor; for other depths, multiply by $\left[\frac{12}{d}\right]^{0.092}$
(7) Do not use 2009 IBC Table 2306.3 or AWC SDPWS with nail spacings less than 6 " on-center. (Studs at boundary locations, where two panels abut, are allowed two rows at 6 " on-center.)
(8) Value accounts for large hole capabilities. See Allowable Holes on page 14.
(9) For $12^{\prime \prime}$ depth. For depths $<31 / 2^{\prime \prime}$, use the $31 / 2$ " factor; for other depths, multiply by $\left[\frac{12}{\mathrm{~d}}\right]^{0.111}$
(10) For column and stud applications, use $\mathrm{F}_{\text {cll }}$ of 500 psi. Alternatively, refer to ESR-1387, Table 1, footnote 15.
(5) Design shear wall applications per 2009 IBC Table 2306.3 or AWC SDPWS. When using
(11) For $11 / 2$ " thick members, use $F_{c \perp}$ of 670 psi in plank orientation. StrandGuard ${ }^{\circledR}$ TimberStrand ${ }^{\circledR}$ LSL sill plate, see the Trus Joist ${ }^{\circledR}$ Treated Sill Plates, Columns, and Studs Technical Brief, TJ-8100.

## Allowable Design Properties (100\% Load Duration)

$11 / 2$ " TimberStrand ${ }^{\circledR}$ LSL Studs
13/4" TimberStrand ${ }^{\circledR}$ LSL Studs

| Design Property | Beam Orientation |  |
| :---: | :---: | :---: |
|  | $\mathbf{1 . 5 5 E}$ |  |
|  | $\mathbf{5 1 / 2 "}$ | $\mathbf{7 1 / 4} \mathbf{" 1}^{\mathbf{\prime \prime}}$ |
| Moment (ft-Ibs) | 1,835 | 3,110 |
| Shear (lbs) | 1,990 | 2,620 |
| Moment of Inertia (in. ${ }^{\mathbf{}}$ ) | 24 | 56 |
| Weight (plf) | 3 | 4.0 |

## $31 / 22^{\prime \prime}$ TimberStrand ${ }^{\circledR}$ LSL Columns and Headers

| Design Property | 1.3E |  |  |  | 1.55E |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Beam Orientation |  | Plank Orientation |  | Beam Orientation |  |  |  |
|  | 51/2" | 71/4" | 51/2" | 71/4" | 51/2" | 71/4" | 91/2" | 117/8" |
| Moment (ft-lbs) | 2,685 | 4,550 | 1,780 | 2,345 | 3,675 | 6,225 | 10,420 | 15,955 |
| Shear (lbs) | 5,455 | 7,190 | 1,925 | 2,540 | 3,980 | 5,245 | 6,870 | 8,590 |
| Moment of Inertia (in. ${ }^{\text {) }}$ | 49 | 111 | 20 | 26 | 49 | 111 | 250 | 488 |
| Weight (plf) | 5.6 | 7.4 | 5.6 | 7.4 | 6 | 7.9 | 10.4 | 13.0 |

## 3½" Parallam ${ }^{\circledR}$ PSL Columns

| Design Property | $\mathbf{1 . 8 E}$ |  |  |  |  | $\mathbf{2 . 0 E}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Beam Orientation |  |  | Plank Orientation |  | Beam Orientation |
|  | $\mathbf{3 1 / 2 "}$ | $\mathbf{5 1 / 4 "}$ | $\mathbf{7 "}$ | $\mathbf{5 1 / 4 "}$ | $\mathbf{7 "}$ | $\mathbf{9 1 / 4 \mathbf { 4 }}$ |
| Moment (ft-lbs) | 1,640 | 3,670 | 6,320 | 2,460 | 3,275 | 12,415 |
| Shear (lbs) | 1,550 | 2,820 | 3,755 | 2,330 | 3,105 | 6,260 |
| Moment of Inertia (in. ${ }^{\mathbf{4}}$ ) | 13 | 42 | 100 | 19 | 25 | 231 |
| Weight (plf) | 3.8 | 5.7 | 7.7 | 5.7 | 7.7 | 10.1 |

## 514" Parallam ${ }^{\circledR}$ PSL Columns and Headers

| Design Property | 1.8E |  |  | $\mathbf{2 . 0 E}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Beam Orientation |  | Plank Orientation | Beam Orientation | Plank Orientation |
|  | $\mathbf{5 1 / 4 "}$ | $\mathbf{7 "}$ | $\mathbf{7 "}$ | $\mathbf{9 1 / 4}$ | $\mathbf{9 1 / 4} \mathbf{" 1}^{\mathbf{\prime \prime}}$ |
| Moment (ft-Ibs) | 5,285 | 9,485 | 7,050 | 18,625 | 10,285 |
| Shear (lbs) | 3,490 | 5,635 | 4,655 | 9,390 | 6,800 |
| Moment of Inertia (in.4) | 63 | 150 | 84 | 346 | 112 |
| Weight (plf) | 8.6 | 11.5 | 11.5 | 15.2 | 15.2 |

## 7" Parallam ${ }^{\circledR}$ PSL Columns

| Design Property | 1.8E | 2.0E |
| :---: | :---: | :---: |
|  | Beam Orientation | Plank Orientation |
|  | $7^{\prime \prime}$ | $\mathbf{9 1 / 4}$ |
| Moment (ft-lbs) | 12,140 | 17,710 |
| Shear (lbs) | 6,205 | 9,065 |
| Moment of Inertia (in.4) | 200 | 264 |
| Weight (plf) | 15.3 | 20.2 |

## Beam Orientation


Column Orientation


Plank Orientation


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[^2]
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[^3]
[^0]:    (1) Listed heights are distances between points of lateral support placed perpendicular to the plane of the wall.

[^1]:    * Applies to stud applications other than $2 \times 4$ and $2 \times 6$ studs in conventional construction as shown on page 3.

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